## HETERODYNE DETECTION OF SAW-MODULATED LIGHT WAVES<sup>1)</sup>

HOFMANN, H.,2) SEIFERT, U.,2) Dresden

For applications of integrated optic in communication systems the interaction of Surface Acoustic Waves (SAW) and light waves is an important method for signal processing. The paper deals with the heterodyne detection of modulated light by use of SAW on LiNbO<sub>3</sub>-integrated optical devices; experimental results are given.

### I. INTRODUCTION

The development of Broad—Band—Fibre—Optical communication-systems requires new methods of light-modulation, in order to utilize better the great brandwidth of light (10<sup>14</sup> Hz). Besides the earlier existing intensity — modulation we also have to employ phase- and frequency-modulation of light. A method to receive frequency-modulated optical signals is the heterodyne detection, which has been known since 1930 for receiving broadcasting signals. In the optical communication technique it is possible to modulate light with

an integrated optical Bragg-modulator, which works with Surface Acoustic Waves (SAW) and afterwards receives the light through heterodyne detection. This paper deals with the Bragg-modulation of light and the heterodyne detection of a frequency-modulation-signal.

### II. BRAGG-MODULATOR

For modulation of guided optical waves we applied an integrated optical Bragg-modulator on the basis of LiNbO<sub>3</sub>. (Fig. 1)

On the left the light is guided by a Titanium-doped LiNbO<sub>3</sub>-waveguide On the left the light is guided by a Titanium-doped LiNbO<sub>3</sub>-waveguide (monomode light from He—Ne-LASER, wavelength 0.6328 µm). There we have the interdigital transducer (IDT), which has produced the SAW. The SAW forms a phase-lattice in the interaction-zone and the guided light is diffracted.

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Technische Universität Dresden, Informatikzentrum, Mommsenstrasse 13, 8027 DRESDEN, DDR

When the angle between the guided optical wave and the SAW is the Bragg-angle

$$\Theta_B = \arcsin \frac{m \cdot \lambda_L}{2n_f \Lambda_{SAW}},$$

 $\Xi$ 

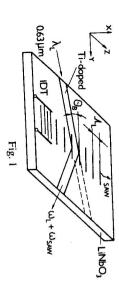
LASER

bulk - wave - modulator

 $\lambda_L = \text{wavelength of light}; \quad \Lambda_{SAW} = \text{wavelength of SAW}; \quad n_f = \text{Break-index}$ (=2.28); m = order of diffraction, then all the energy would be deflected in the first order m = 1. Besides the frequency of light  $\omega_B$  changes according to formula  $\omega_B = 0.1 + 0.00$ 

$$\omega_B = \omega_L \pm \omega_{SAW}$$

 $\omega_L$  = frequency of the input light.



Because the SAW is propagated in one direction, we have the doppler-effect and only "plus" in the formula (2). The Bragg-modulator is a single-sideband-frequency-modulator.

## III. HETERODYNE DETECTION

A direct detection of frequency-modulated light is not possible, because a simple Avalanche-Photodiode integrates over the power of light. For frequency-detection therefore the light is mixing in a heterodyne detector by heterodyning the received light with the light of the local oscillator and the heterodyning alternation device (fotodiode).

mixing at a nonlinear optical device (totodiode). Compared with direct detection we get by the heterodyne detection a greater signal power. By direction the signal coursent  $i_{SD}$  is proportional to the optical

signal power P

$$i_{SD} = k_1 * P \tag{3}$$

but by heterodyne detection the signal current  $i_{SH}$  is also dependent on the power

of the local oscillator  $P_{LO}$ 

$$i_{SH} = k_2 * \sqrt{P_{LO}} * P.$$

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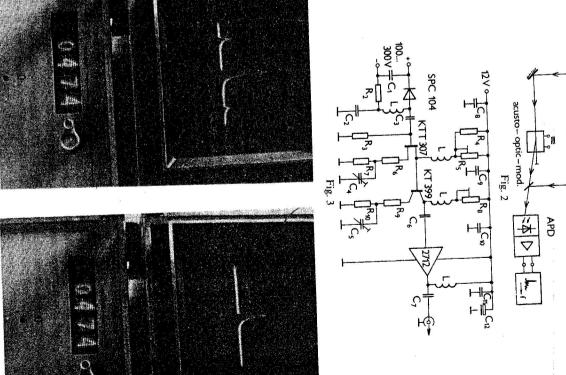


Fig. 5. The spectrum of the heterodyne detected signal

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Fig. 4. The spectrum of the direct detected signal

current at the output of the heterodyne detector will be higher. It is possible to use high power of a local oscillator, and therefore the signal

bulk-wave-modulator. This reference-bulk-wave-modulator produces the reoptical detector with the electronic amplifier. the mixing of the signals  $\omega_{Bragg} + \omega_{reference}$ . Fig. 3 shows the electric circuit of the both beams fall in the Avalanche diode and we get at the output of the amplifier from the He-Ne-LASER enters the Bragg-modulator and at the bottom the ference—frequency—signal (like the local oscillator). Over a transparent mirror Fig. 2 shows the optical circuit of the heterodyne detector. At the top the light

Fig. 4 and Fig. 5 show the results of detection by a spectrum analyser.

#### IV. CONCLUSION

cy-multiplexing) and in measuring methods (Gyroscopy, Spectroscopy). preparing a better Bragg-modulator with a Chirp-Interdigital-Transducer and dyne detector find applications in communication systems (especially frequen-Horn-structure of the lightwaveguide. The Bragg-modulator and the hetero-This arrangement has little efficiency of diffraction, but currently we are

Bragg-modulator and the heterodyne detector. At the Technical University of Dresden we work on the improvement of the

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# ГЕТЕРОДИННОЕ ИЗМЕРЕНИЕ ПАВ — МОДУЛИРОВАННЫХ СВЕТОВЫХ ВОЛН

сигналов. Работа посвящена гетеродинному измерению модулированного света при помощи акустических волн (ПАВ) со световыми волнами является важным методом для обработки ПАВ на LiNbO3 интегральных оптических устройствах. Приведены экспериментальные ре-В применениях интегральной оптики и системах связи взаимодействие поверхностных