## PHASES IN THE PRODUCTS OF THE REACTION OF SULPHUR HEXAFLUORIDE WITH COPPER

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phases should comply with the Gibbs phase rule. therefore necessary to concentrate on the selection of phases, since the number of is thus heterogeneous, and on determining the composition of the system it is of 298.15 K to the boiling temperature of copper. The system of the reaction products of pressures of 0.101325-2 MPa and temperatures ranging from room temperature The purpose of this paper is to follow the interaction of SF<sub>6</sub> with Cu in the region

#### I. INTRODUCTION

contain copper. SF<sub>6</sub> reacts with Cu already at temperatures of about 100 °C [1] breakers filled with sulphur hexafluoride — SF<sub>6</sub> are made of copper or may Some inner components of high voltage and very high voltage circuit

substances briefly denoted ( $SF_6 + mCu$ ), which may be present in the products of the reaction of one mole SF<sub>6</sub> with m moles of Cu after chemical equilibrium has been attained temperature. The products of the interaction form a system of individual chemical equilibrium of the system in the ideal state, at constant pressure and The interaction of SF<sub>6</sub> with Cu should be studied from the viewpoint of the

### II. DESCRIPTION OF THE SYSTEM

condensed components S [2], Cu, CuF, CuF<sub>2</sub> [3], CuS, Cu<sub>2</sub>S [4]. SF<sub>3</sub>, SF<sub>2</sub>, SF, S, S<sub>2</sub>, S<sub>3</sub>, S<sub>4</sub>, S<sub>5</sub>, S<sub>6</sub>, S<sub>7</sub>, S<sub>8</sub>, F [2], Cu, Cu<sub>2</sub>, CuF, CuF<sub>2</sub> [3], and the potential  $\Phi^0(T)$  are available in literature. They include the gases SF<sub>6</sub>, SF<sub>5</sub>, SF<sub>4</sub>. system — whose heats of formation  $\Delta_f H^0$  and the values of the thermodynamic We took into consideration all possible compounds — components of the

Gases form a single phase, it is supposed that the condensed components

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form an independent phase. The number of phases in the system which is in equilibrium must be in harmony with the phase rule. The phase rule indicates the number of the degrees of freedom of the system; the number of the degrees of freedom is the number of the degrees of freedom is thus given by the difference of the number of all variables of the system (at constant temperature and pressure it is the composition of the system) and the number of the additional independent conditions which the system must satisfy. According to [5] the number of the freedom degrees equals M - h - a, where M is the number of the chemical elements forming a system, h is the number of phases, and a is the number of additional independent conditions. The use of the phase rule always implies a certain degree of uncertainty, as we do not know whether we have determined the number of conditions correctly [5]. The states characterized by the negative value of the number of freedom degrees are unrealizable. From the phase rule it follows that

$$h \le M$$
. (1)

The system (SF<sub>6</sub> + mCu) is formed by S, F, Cu, i.e. M = 3. The amounts of the components are successively denoted by the symbols  $n_1, n_2, ..., n_{25}$ . According to (1) there are at most three phases in the system. It means that in case of the presence of a gaseous phase there can be two condensed phases at the most, i.e. there can be only two non-zero amounts in the equilibrium among  $n_{20}, n_{21}, n_{22}, n_{23}, n_{24}, n_{25}$ .

At constant temperature and pressure the Gibbs energy of the system is the function of the composition  $n_1, n_2, ..., n_{25}$  and the equilibrium composition minimizes the Gibbs energy. This fact forms the basis of the calculation method of the equilibrium composition [6] used for the calculation of the composition of the system (SF<sub>6</sub> + mCu).

The amount of Cu in the system is represented by the parameter m, whose value is in the range from zero to 5.4 mol. In  $(SF_6 + 5.4 \text{ Cu})$  70% of the total mass goes to copper. In  $(SF_6 + m\text{ Cu})$  no presence of ions is presumed as their molar fractions at the boiling temperature of copper are lower than  $10^{-4}$  and thus cannot influence the occurrence of condensed compounds in the system.

# III. DISCUSSION OF THE RESULTS

In calculating the composition of  $(SF_6 + mCu)$  the occurrence of a gaseous phase was always assumed. The occurrence of condensed phases in dependence on temperature T and on the amount of copper m  $(0 \le m \le 5.4)$  at the pressure p = 1 MPa is well perceptible from Fig. 1. The curves in Fig. 1, together with

the coordinate axes, divide the first quadrant of the coordinates m, T into bounded areas of couples (m, T). The condensed phases occurring in  $(SF_6 + mCu)$  in the respective area are written in Fig. 1. The initial and final points of some curves in Fig. 1 are marked with the capital letters of the alphabet. The position of the curves AB, CD, EZ, HL, FZ, ZI, ZK depends on the pressure; with increasing pressure the curves are shifted towards higher temperatures. The temperature corresponding to point B is the boiling temperature of sulphur for p = 1 MPa. In the line segment CD CuS/c decomposes to  $Cu_2S/c$  and to S/g [7]. Above the temperature corresponding to points E and H, respectively, there arises a vapour of  $CuF_2$  and CuF in a considerable amount. In a similar way  $Cu_2S$  decomposes at temperatures above the point F.

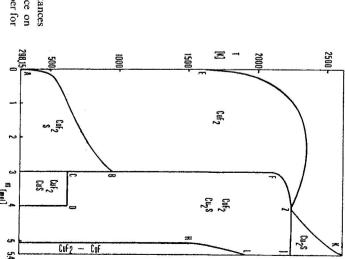
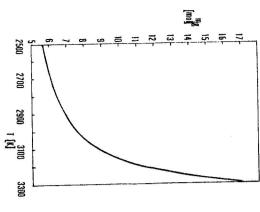


Fig. 1. The occurrence of condensed substances in the  $(SF_6 + mCu)$  system in dependence on the temperature and the amount m of copper for p = 1 MPa

It is necessary to remark that in the system we do not assume the presence of  $\text{Cu}_2\text{S}/g$ , for which the values  $\Phi^0(T)$ ,  $\Delta_r H^0$  lacked, and the data upon the decomposition or evaporation of  $\text{Cu}_2\text{S}/c$ . For this reason we should take with reserve also the position of curve ZK. Very interesting is the information concerning the decomposition of  $\text{CuF}_2/c$  to CuF/c at the melting temperature

of CuF<sub>2</sub>/c (1223 K) [8]. Calculations did not confirm this fact. Besides, [8] expresses doubts concerning the existence of CuF/c.

It follows from the results of the calculations that the decomposition  $SF_6$  is caused by copper. During the decomposition of  $SF_6$  there arise fluorine and sulphur and practically the whole content of copper reacts with them. We should add that the boiling temperature of copper for the pressure of 1 MPa equals 3454 K. Condensed copper appears in the system only for m > 5.4 mol. The maximum amount  $m_g$  of copper appearing in the gaseous components of the system increases with temperature. This dependence is illustrated in Fig. 2 for p = 1 MPa. With increasing pressure the curve in Fig. 2 is shifting towards lower amounts.



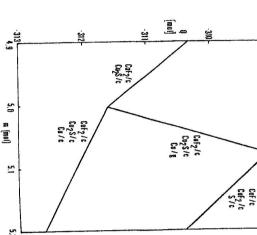


Fig. 2. Temperature dependence of the maximum amount  $m_g$  of copper in the gaseous phase of the system for p = 1 MPa

Fig. 3. The graph of function Q in the neighbourhood of the phase transition for p = 1 MPa

If a constant m is given  $(0 \le m \le 5.4)$ , it is necessary, when interpreting the results of the equilibrium calculation, to take into account the rate of the chemical reactions at the temperature changes. More complicated is the interpretation of the calculation in the case of constant temperature and of a changing m. Let us denote Q = G/RT, where G is the Gibbs energy of the system

in equilibrium at the given temperature and pressure (R is the gas constant). The equilibrium composition as well as the calculation of the values Q = Q(m) is the result of a numerical process, unstable for some values of m, e.g. for  $m_1, m_2, \ldots$  At the points  $m_1, m_2, \ldots Q(m)$  apears either as a discontinuous function or is increasing in the neighbourhood of these points. For other values of m ranging from zero to 5.4 Q(m) is a decreasing function. The points  $m_1, m_2, \ldots$  will be further regarded as points of discontinuity and at a limiting transition we shall take into account only the points in which Q(m) is decreasing. If m is nearing the value 3 from the left  $(m \to 3-)$  and the temperature is below point B, then

$$SF_6 + 3Cu \rightarrow 3CuF_2/c + S/c$$

In the system the gaseous phase disappears, while for  $m \rightarrow 3 +$ 

$$SF_6 + 3Cu \rightarrow 3CuF_2/c + S/g$$

where in S/g we have included the molecules  $S_1,\,S_2,\,S_3,\,S_4,\,S_5,\,S_6,\,S_7,\,S_8.$  The difference

$$\lim_{m\to 3+} Q(m) - \lim_{m\to 3-} Q(m)$$

equals the difference of the Q values for S/g and S/c. The difference decreases with increasing temperature and above the boiling temperature of the sulphur equals 0. Similarly below point D for  $m \to 4$ —

$$SF_6 + 4Cu \rightarrow 3CuF_2/c + CuS/c$$

for  $m \rightarrow 4 +$ 

$$SF_6 + 4Cu \rightarrow 3CuF_2/c + 0.5Cu_2S/c + 0.5S/g$$
.

Finally below point H for  $m \rightarrow 5$  – there is

$$SF_6 + 5Cu \rightarrow 3CuF_2/c + Cu_2S/c$$

for  $m \rightarrow 5 +$ 

$$SF_6 + 5Cu \rightarrow CuF_2/c + 4CuF/c + S/g.$$

At each of the above points of discontinuity the limit of function Q(m) from the right is always higher than the limit from the left. The minimum value of the function Q corresponds to the state of equilibrium. This might mean that with increasing m the system will reach the first point of discontinuity and the additional copper will not react. At the point of discontinuity the gaseous phase will completely disappear, the additional copper will evaporate as the equilibrium composition is calculated at constant temperature and pressure and the given pressure 1 MPa can be formed with gaseous copper. As an example in Fig.

corresponding phases are indicated. m = 5 mol for p = 1 MPa and T = 800 K. In branch every of the graph the 3 we can see the graph of the function Q(m) in the neighbourhood of the point

#### IV. CONCLUSION

agrees with the Gibbs phase rule, depends on the amount m of copper and is and pressures taken into consideration. The maximum amount  $m_g$  of Cu appearevident from Fig. 1. The occurrence of the condensed substances in the reaction products, which at constant temperature and pressure that SF<sub>6</sub> reacts with Cu at all temperatures The system of the reaction products is heterogeneous for lower temperatures. illustrated in Fig. 2 in dependence on the temperature for higher temperatures. ing in the gaseous components of the reaction of Cu with one mole of SF6 is It follows from the results of the calculation of the equilibrium composition

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# ФАЗЫ В ПРОДУКТАХ РЕАКЦИИ SF, С Cu

от 0,101325 до 2 МРа и в области температур, пробегающих от комнатных ее значени поскольку число фаз должно подчиняться правилу фаз Гиббса (298,15 К) до температуры кипения меди. Система продуктов этой реакции является неод нородной, поэтому для определения ее состава необходимо сосредоточиться на выборе фаз Целью настоящей работы является изучение взаимодействия  ${
m SF}_6$  с  ${
m Cu}$  в области давлени