# THE INTERACTION OF PLASMA WITH A SOLID SURFACE\*

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A theory describing the interaction of plasma with a solid surface is formulated. An infinite plasma interacting with an infinite planar wall was chosen as a model for theoretical considerations. A flux of charged particles to the wall in ambipolar approximation was calculated as a first step. Equations describing an electrostatic sheath are presented taking into account heating, variation of the ioh mobility and the electron-ion recombination. Boundary conditions are studied in more detail when particles can be emitted or reflected at the wall surface.

# взаимодействие плазмы с твёрдой поверхностью

В работе сформулирована теория, описывающая взаимодействие плазмы с твёрдой поверхностью. В качестве модели для теоретического рассмотрения была выбрана бесконечная плазма, взаимодействующая с бесконечной плоской стенкой. В амбиполярном приближении рассчитан поток заряжённых частиц, падающих на стенку. Приведены уравнения, описывающие электростатическую оболочку с учётом нагрева, изменения подвижности ионов и электрон-ионной рекомбинации. Более подробно изучены граничные условя для случая, когда частицы могут испускаться поверхностью стенки или же от неё отражаться.

#### I. INTRODUCTION

The plasma treatment of solid material is based on the interaction of particles present in the plasma with a target surface. Near the wall the properties of plasma change entirely, since an electrostatic sheath adjacent to the solid surface is formed. In this region the condition of quasineutrality must fail since to balance ion and electron fluxes to the wall the ion concentration must exceed the electron concentration by a factor equal to the ratio of their normal velocities at the wall. It is clear that the interaction of the plasma with the solid surface is strongly influenced by the properties of the region close to the wall.

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boundary conditions with respect to properties of the solid surface. flux density and velocity of charged particles when striking the surface, and the In the present paper we aim at finding information about the sheath, namely, the

### II. A PLASMA MODEI

a onedimensional basis. the theoretical consideration which enables us to formulate the problem on infinite plasma interacting with an infinite planar wall can be used as a model for recombination must be taken into consideration. Then as a good approximation an In many applications the plasma dimensions are so large that the electron-ion

production rate of the charged particles can be written as When  $\alpha$  is the ionization rate and  $\beta$  the recombination coefficient, the

$$\frac{\delta n_{+}}{\delta t} = \frac{\delta n_{-}}{\delta t} = \alpha n_{-} - \beta n_{-} n_{+} , \qquad (1)$$

where  $n_+$  and  $n_-$  are the number densities of ions and electrons, respectively. In the plasma far from the wall quasineutrality is present and number densities of electrons and ions are the same, and reach the equilibrium number density

$$n_{+} = n_{-} = n_{0} = \alpha/\beta$$
 (2)

# III. FLUX OF CHARGED PARTICLES TO THE WALL IN AMBIPOLAR APPROXIMATION

surface is made of insulator or it is held at the floating potential). Then the charged equation  $(n = n_+ = n_-)$ particles move to the wall by ambipolar diffusion which can be described by the In this approximation no net current is supposed to flow to the wall (the solid

$$-D_a \frac{\mathrm{d}^2 n}{\mathrm{d}z^2} = \frac{\delta n}{\delta t} \,. \tag{3}$$

planar wall. Insertion of (1) into the last equation yields Here  $D_a$  is the ambipolar diffusion coefficient and z is the coordinate normal to the

$$\frac{D_n}{n_0 \alpha} \frac{d^2 n}{dz^2} = -\frac{n}{n_0} + \left(\frac{n}{n_0}\right)^2. \tag{4}$$

Integration of this equation yields the result

$$\frac{D_a}{n_0^2 \alpha} \left( \frac{dn}{dz} \right)^2 = \frac{1}{3} + \frac{2}{3} \left( \frac{n}{n_0} \right)^3 - \left( \frac{n}{n_0} \right)^2, \tag{5}$$

where we have assumed that dn/dz = 0 for  $n = n_0$ . This result can be written as  $(\Lambda^2 = D_a/\alpha)$ 

$$dz = -\frac{\Lambda}{n_0} \sqrt{3} \left[ \left( 1 - \frac{n}{n_0} \right) \left( 2 \frac{n}{n_0} + 1 \right)^{1/2} \right]^{-1} dn$$
 (6)

and integrated again for the boundary condition n = 0 at the wall (z = 0)

$$\frac{z}{\Lambda} = -\ln\left[\frac{\sqrt{3}-1}{\sqrt{3}+1}\frac{\sqrt{3}+\left(2\frac{n}{n_0}+1\right)^{1/2}}{\sqrt{3}-\left(2\frac{n}{n_0}+1\right)^{1/2}}\right].$$
 (7) ted in Fig. 1 together with the flux density of the charged particles

The result is plotted in Fig. 1 together with the flux density of the charged particles

$$j = -D_a \frac{dn}{dz} = n_0 \left(\frac{\alpha D_a}{3}\right)^{1/2} \left(1 - \frac{n}{n_0}\right) \left(2 \frac{n}{n_0} + 1\right)^{1/2}.$$
 (8)

The flux density at the wall is given by

$$j_{w} = n_{0} \left( \frac{\alpha D_{a}}{3} \right)^{1/2} = n_{0}^{3/2} \left( \frac{D_{a} \beta}{3} \right)^{1/2}. \tag{9}$$

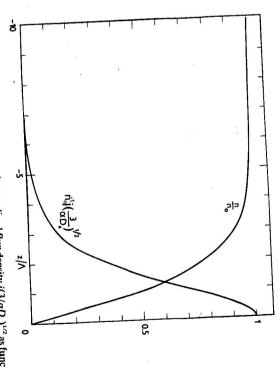


Fig. 1. Normalized number density  $n/n_0$  and normalized flux density  $j(3/\alpha D_a)^{1/2}$  as functions of normalized distance z/A in the ambipoar approximation

#### IV. SHEATH

[1-5]). Unfortunately, the progress that has been made so far as regards the problem of a plasma sheath near the wall has long been studied (see for example The ambilopar approximation cannot give any information about the sheath. The

135

electron-ion recombination will be also taken into consideration. conception of Forrest and Franklin [6] as a starting point. In our study the theory is still subject to several restrictions. In the present paper we have used the heating of positive ions, variation of the ion mobility in the electric field and

Poisson's equation describes the electrostatic field produced by a charge

$$\frac{\mathrm{d}^2 \Phi}{\mathrm{d}z^2} = -\frac{e}{\varepsilon_0} \left( n_+ - n_- \right),\tag{10}$$

electrostatic potential. The generation of charged particles is given by the continuiwhere e is the elementary charge,  $\varepsilon_0$  the permittivity of free space and  $\Phi$  the

$$\frac{\mathrm{d}}{\mathrm{d}z}(n_+V_+) = \frac{\delta n_+}{\delta t}; \quad \frac{\mathrm{d}}{\mathrm{d}z}(n_-V_-) = \frac{\delta n_-}{\delta t}. \tag{11}$$

By using (1) and integrating we have

$$n_+V_+ - n_-V_- = i_w/e$$
, (12)

where i, is the net electric corrent density at the wall

The momentum equation for the positive ions can be written as [7]

$$V_{+} \frac{dV_{+}}{dz} = -\frac{e}{m_{+}} \frac{d\Phi}{dz} - \frac{1}{n_{+}} \frac{d}{dz} (n_{+} < c_{z}^{2} >) - \nu_{+} V_{+} - V_{+} \frac{1}{n_{+}} \frac{\delta n_{+}}{\delta t}.$$
 (13)

momentum transfer. the z component of the random velocity and  $v_+$  the collision frequency for the Here  $V_{+}$  and  $V_{-}$  are drift velocities of charged particles,  $m_{+}$  the mass of the ion,  $c_{i}$ 

the collision frequency can be written as follows [8] with the drift velocity of the ion. For a special case of the constant mean free path The collision frequency is either a constant (constant mean free time) or it varies

$$v_{+} = v_{+0} \left( 1 + a m_{+} V_{+}^{2} / k T_{g} \right)^{1/2},$$
 (14)

a numerical factor determined by the natura of the ion-atom interaction. The where  $v_{+0}$  is the "zero-field" collision frequency,  $T_a$  the gas temperature and random energy [8] heating of positive ions in the electric field is described by the z component of the

$$m_+\langle c_z^2\rangle = kT_q + \gamma m_+ V_+^2, \qquad (15)$$

where  $\gamma$  is a numerical factor.

considering the fact that the electron drift velocity is much smaller than the random Similarly, we can also write the momentum equation for the electrons. But,

velocity of electrons, the electron density very nearly satisfies the Boltzmann

relation [8, 9] 
$$n/n_0 = \exp(e\Phi/kT_-). \tag{16}$$

The numerical solution of this problem is presented in [10].

### V. BOUNDARY CONDITIONS

strike the wall the z component of the particle velocity of the drift V, and the random velocity c must be a positive one. The flux density of the striking particles Now we try to study the processes at the solid surface in more detail. In order to

$$j_s = 2\pi \int_0^{V_w} \int_0^{\pi} (V_w + c \cos \delta) c^2 f(c, \vartheta) \sin \vartheta \, d\vartheta \, dc + \tag{17}$$

$$+2\pi \int_{v_{\omega}}^{\infty} \int_{0}^{\phi_{m}} (V_{\omega} + c \cos \theta) c^{2} f(c, \theta) \sin \theta d\theta dc$$

where  $\vartheta_m$  must obey the following relation

$$V_{m} + c \cos \theta_{m} = 0.$$

(18)

As the velocity distribution is axially symmetric, the distribution function f does not

and nonreflecting walls  $j_r = 0$ . Generally, the wall can reflect failling particles and flux density of the particles with a negative velocity at the wall. For nonemitting depend on the variable  $\varphi$ . their emission is also possible. Then we have The flux density at the wall due to the drift is  $j_w = j_i + j_i$ , where  $j_i$  represents the

$$j_r = -\kappa j_s - j_e$$
 and  $j_w = (1 - \kappa) j_s - j_e$ ,

where  $\varkappa$  is the reflection coefficient and  $J_E$  the flux density of the emitted particles. The formulae (17), (18) and (19) represent the boundary conditions in the most

the distribution function f is supposed to be independent of  $\vartheta$ . The formula (17) In order to understand these conditions we make a rough approximation when

can be integrated over  $\vartheta$  to give

in be integrated over 
$$c$$
 or  $c$  or

In the limit where the random velocity of particles is very much greater than the

drift velocity we may put  $V_* \rightarrow 0$ . Then

$$j_s = \frac{1}{2} n_w V_w + \frac{1}{4} n_w \langle c \rangle , \qquad (21)$$

where  $\langle c \rangle$  is the mean speed. The drift velocity at the wall is given by

$$V_{w} = \frac{1}{2} \frac{1-x}{1+x} \langle c \rangle - \frac{j_{e}}{2(1+x)}.$$
 (22)

(21) yields the familiar results [11] In a special case when the drift of particles is controlled only by diffusion, equation

$$j_s = \frac{1}{4} n_w \langle c \rangle - \frac{1}{2} D \frac{dn}{dz}$$
 (23)

random velocity, we may put  $V_{*} \rightarrow \infty$ . Then In case of the reverse limit, when the drift velocity is large in comparison with the

$$j_s = n_w V_w = j_w \tag{24}$$

and the boundary condition has the form

$$x_{J_m} + J_e = 0. (25)$$

Therefore, the last case can occur only for nonemitting and nonreflecting walls. As x,  $j_{*}$  and  $j_{*}$  must be positive numbers or zero, we get  $j_{*}=0$  and  $xj_{*}=0$ .

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