## Letters to the Editor

## REMARK TO THE CASSON EQUATION

## SYLVIA PULMANNOVÁ\*, Bratislave

terials: printing inks [1], molten chocolate [2], human blood [3, 4]. gates of different lengths. This equation was experimentally verified for different mawhich the attractive forces act. Owing to these forces, the particles form rod-like aggrenally derived for the rheological model of a suspension of rigid spherical particles, among Casson's law [1] for the relation between shear stress and velocity gradient was original

diameter) of the rod-like aggregates is a linear function of the  $y=(\eta_0 D)^{-1/2}$  ( $\eta_0$  is the viscosity of the suspending liquid and D is the velocity gradient), that is Casson assumed that the axial ratio j (that is the ratio of the rod length to the particle

$$j = \alpha + \beta y . (1)$$

a single particle, which is valid for the great velocity gradients, and  $j=\beta(\eta_0 D)^{-1\beta}$ , which is valid for low values of D. This relation is a generalization of the relations  $j=j_0$ , where  $j_0$  is the axial ratio of

The resultant relation between F and D is then

$$F^{1/2} = k_0 + k_1 D^{1/2}, (2)$$

where F is the shear stress.

A special generalized form of (1), which has also practical meaning, is

$$j = \alpha + \beta y^{\sigma}, \tag{3}$$

from which we can obtain, in an analogical way as that used by Casson

$$F^{r/2} = k_0 + k_1 D^{r/2} \,. \tag{4}$$

Let us substitute into the equation

$$\eta = \eta_0(1-c) + \eta_0 ajc,$$

(c is the volume concentration), obtained by Casson, relation (3) instead of (1). Thus

$$\eta = \eta_0(1-c) + \eta_0 a\alpha c + \frac{a\beta c}{D^{1/2}} \eta_0^{(1-\tau/2)}.$$
 (5)

Relation (5) can be applied only to very diluted suspensions. Casson generalized it in

sion. By (5) the viscosity of the new suspension is sion  $\eta$  can be considered as the viscosity of the suspending medium of the new suspenthe original suspension. The whole concentration of the new suspension is  $c^* = c(1-\delta c) +$ volume being  $\delta c$  to every  $(1 - \delta c)$  volume unit of the original suspension. Suppose that the new suspension is a very diluted suspension with the volume concentration & of +  $\delta c$ , that is  $\delta c = dc/(1-c)$ , where  $dc = c^* - c$ . The viscosity of the original suspen-Let us consider a small addition of the solid material to the suspension, the added

$$\eta' = \eta[1 + (a\alpha - 1)\delta c] + \frac{a\beta\delta c}{D^{r/2}}\eta^{(1-r/2)}$$
 (6)

and for  $d\eta = \eta' - \eta$  we have

$$d\eta = \left[ \eta(a\alpha - 1) + rac{\eta^{(1-r/2)}}{D^{r/2}} a eta 
ight] rac{dc}{(1-c)} \, .$$

3

Then we obtain

$$\frac{d\eta}{A\eta + B\eta^{(1-\tau/2)}} = \frac{dc}{1-c},$$

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when ax-1=A and  $a\beta/D^{r/2}=B$ . By integrating this equation with the boundary condition  $\eta=\eta_0$  at c=0, we obtain

$$\eta'^{\prime} = \left[rac{\eta_0}{(1-c)A}
ight]^{ au/2} + rac{B}{A}\left[\left(rac{1}{1-c}
ight)^{A au/2} - 1
ight].$$

(9)

We obtain the relation between F and D multiplying by  $D^{r/2}$ 

$$F^{r/2}=k_1D^{r/2}+k_0$$
,

where

$$k_1 = \left[\frac{\eta_0}{(1-c)A}\right]^{\eta_2^2}, \quad k_0 = \frac{a\beta}{A}\left[\left(\frac{1}{1-c}\right)^{A/2} - 1\right].$$
 (10)

For example, for r = 2, we obtain the equation

$$F=k_1D+k_0\;,$$

(11)

that is the Bingham relation for the plastic flow [5].

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<sup>\*</sup> Ústav teórie merania SAV, Bratislava, Dúbravská cesta.

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